CHAPTER 8 LEAD ASSESSMENT

A

Jack

al Car

CHAPTER 8.1 INTRODUCTION AND METHODS

Bachter

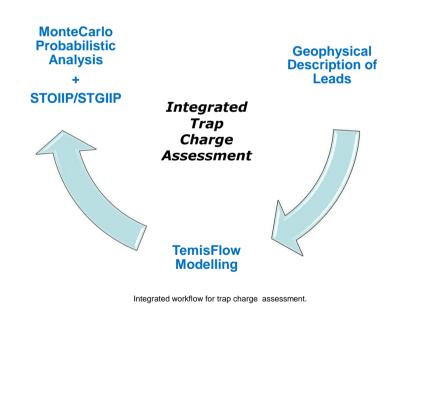
#### Central Scotian Slope Study – CANADA – June 2016

#### Integrated Trap Charge Assessment

The traditional approach for estimating in place hydrocarbon volumes consists in solving the STOIIP and STGIIP equations. The total volume of rocks inside the lead perimeter, the percentage of that volume that could correspond to reservoir rocks (NTG), the average porosity and hydrocarbon saturation are the main inputs considered in these equations. The main uncertainties of this method are often related to the hydrocarbon charge and composition. There is no simple way to estimate trap charge and hydrocarbon composition without numerical models of expulsion and fluid migration.

For this reason the approach retained for the lead assessment consists in coupling the volumetric approach mentioned above with a numerical model of the petroleum system using TemisFlow<sup>TM</sup>. This integrated method allows first a good approximation to the maximum storage capacity of leads based on seismic interpretation and geological models, and second a good comprehension of the type of hydrocarbons, migration pathways and trapping mechanisms from the TemisFlow results.

The hydrocarbon fractions considered for each lead are extracted from TemisFlow™ allowing the discrimination of gas prone and oil prone accumulations at the different stratigraphic levels. Finally, a number of MonteCarlo probabilistic simulations were generated to take into account uncertainties related to entrapped volumes.



# The two methodologies for the leads assessment, conventional geophysical methods and the basin modelling approach are described on the following page.

For the basin modelling, migration simulations (calculation of HCs and water movements within the porous media) are performed using Full Darcy capabilities of TemisFlow<sup>™</sup> in a 2 km \* 2 km grid with a high vertical resolution. The volumetric calculations for the leads results from the redistribution of migrated HC in a 1 km \* 1 km grid using the Trap Charge Assessment tool in TemisFlow<sup>™</sup>. The redistribution is based on topographical analysis (in terms of flow lines and drainage areas – Ray Tracing approach) of the top horizon of the analyzed layer/play (Chapter 7, PL. 7.3.1). A definition of thresholds for hydrocarbon fluids concentration (in terms of masses) is provided, thresholds below which hydrocarbon quantities are discarded from the volumes computation as they are considered as non-pay.

For the geophysical methods, two scenario have been defined, which are detailed on the next page:

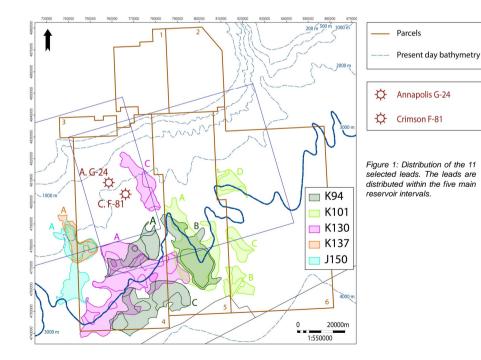
- A scenario in which generated hydrocarbons are only Gas and Condensate (Scenario 1)
- A scenario in which generated hydrocarbons are Oil and Gas (Scenario 2)

It is important to note that the geophysical component focuses on what is considered to be the top 11 leads (Figure 1). TemisFlow<sup>™</sup> modelling allows for a verification of selected leads and gives volumes of oil and gas for each stratigraphic play within each parcel. It is also important to note that the geophysical approach gives only a partial view of the resource potential, whereas TemisFlow<sup>™</sup> results allow assumptions regarding the total trapped volume, as well as the type of hydrocarbon trapped and ratio between the different phases.

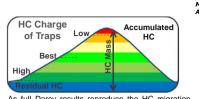
A summary of the total volume for the 11 leads is presented in Table 1.

Leads	Gas	Boe Gas	Oil	Boe
Summary	Tcf	MMbbl	MMbbl	MMbbl
Scenario (1) Gas & Condensate	45	7720	4334	12054
Scenario (2) Oil & Gas	52	9039	2229	11267

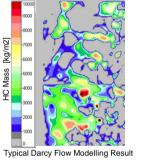
Table 1: Summary of the leads Oil and Gas total volume for each scenario.

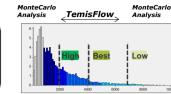


Central Scotian Slope Study – CANADA – June 2016



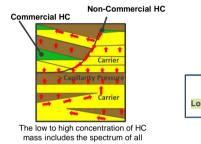
As full Darcy results reproduce the HC migration through porous media HC mass is represented by continuous low to high values. Low values are most frequent but with less probability of having an efficient migration to the trap's top.





Basin Modelling Methodology for HC Charge Assessment

HC mass distribution typically exhibits an exponential decrease in frequency with concentration.

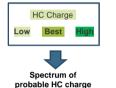


The low to high concentration of H mass includes the spectrum of all the possible HC accumulations in the basin.

A 3D Darcy migration Temisflow Model was generated as reference for the probable "Best" value of HCs trapped at the different reservoir levels. Results include the hydrocarbon volumes in place as well as:

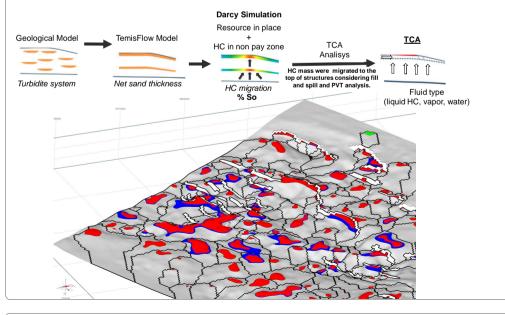
- A detailed description of the HC composition considering HC cracking through time.
- A tracking analysis of the individual supply of source rocks to reservoir levels.

Consequently, raw 3D Darcy migration hydrocarbon quantities trapped within a given layer/play are redistributed using the Trap Charge Assessment tool (TCA) available in TemisFlow. Low and High values were estimated by coupling Temis results with a statistical MonteCarlo analysis.

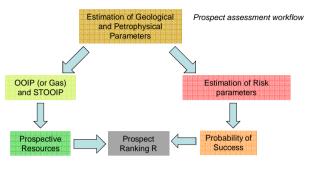


scenarios

The HC redistribution is based on a geometric analysis (in terms of flow lines and drainage areas – Ray Tracing approach) of the top horizon of the reservoir layer/play. This allows identification of all the potential traps in the interval including four or three way closure structures. These structures will then be filled by hydrocarbons trapped at drainage areas considering volume and composition calculated by TemisFlow.

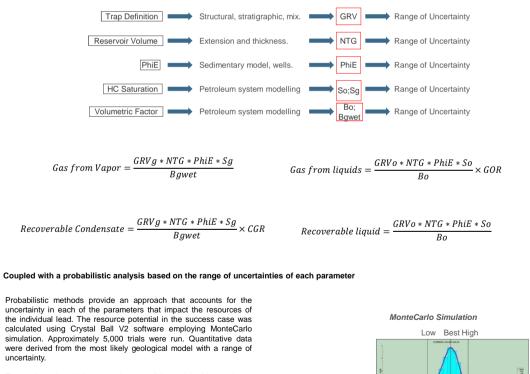


#### Geophysical Methodology for HC Charge Assessment



In order to balance and validate TemisFlow modelling results, a leads assessment was conducted with conventional methods in parallel to the basin modelling stage. Based on the structural maps, 11 large structures within the 5 main reservoir intervals have been identified. They are all located within blocks 4, 5 and 6.

For each lead, two scenarios were simulated: a scenario considering that the lead is filled with gas and associated condensate, and a scenario in which the lead is filled with Oil, Gas and associated condensate. These results are then compared to volumetrics obtained from the TemisFlow modelling results. The convergence of results increases the confidence in the lead prospectivity, whereas values of volume that are different give a range of probability. Volumes estimates are made using the equation and parameters detailed thereafter, however these results do not take into account the recovery factor parameter.



STOIIP Uncertainties

-20%?

These simulations led to an estimation of the unrisked low estimate (P90), best estimate (P50), high estimate (P10) and mean of the prospective resources.



### Introduction and Method

#### Central Scotian Slope Study - CANADA - June 2016

#### Methodology for Lead Risk Assessment and Risking Volumes

The methodology used for the lead risk assessment is based on the CCOP Guidelines for Risk Assessment of Petroleum Prospects. Four parameters representing the major probability factors of discovery are used:

- ✓ Probability of reservoir
- ✓ Probability of seal
- ✓ Probability of trap
- ✓ Probability of hydrocarbon charge

GDE maps are used

for reservoir and seal

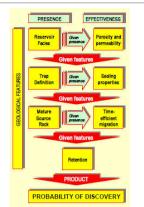
presence.

The probability scale ranges from 0.0 to 1.0 where the end points of the scale: P = 1.0 means 100% certainty and P = 0.0 means 0% certainty.

Seismic data are used for

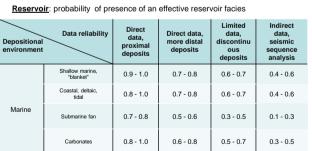
identifying traps, closures,

reservoirs and seals.



Schematic overview of the risking procedure (from CCOP Guidelines for Risk Assessment of Petroleum Prospects. 2000)

Whenever possible, seismic attributes are used to support hypothesis regarding hydrocarbon charge presence.



The major risk identified in the study area is related to the presence/absence of reservoirs, given the uncertainties due to the lack of hard data. Information regarding reservoir effectiveness, saturation and porosity is taken from two CNSOPB reports (Kidson et al., 2002; Kidson et al., 2005) as well as the 2011 PFA study.

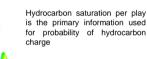
Regarding the probability of seal, overall sealing properties are considered to be acceptable to very good due to:

- the deep water setting of each targeted interval
- the existence of several major MFS such as the Tithonian MFS (J150), the Hauterivian MFS (K130), the Albian/Aptian boundary MFS
- The presence of a well developed salt canopy

The least risk is attributed to the hydrocarbon charge, based on DHI evidence, discoveries in wells, and most importantly. TemisFlow™ modelling results.

Values and criteria used for the risking are detailed in the tables below.

Å



is the primary information used for probability of hydrocarbon

#### Seal: probability of presence of an effective seal mechanism

Seal mechanism			Seal quality	Very Good		Acceptable	Poor
	Top surface	Bottom side	Structural style	good			
Simple	Conform	N/A	Anticline, buried highs, build-ups, faulted str.	0.9 - 1.0	0.8 - 1.0	0.6 - 0.8	0.4 - 0.6
	Uncon -form	N/A	Faulted structures	0.8 - 0.9	0.7 - 0.8	0.5 - 0.7	0.3 - 0.5
	Conform	Uncon -form	Onlap, lowstand wedge	0.5 - 0.7	0.4 – 0.5	0.3 - 0.4	0.1 - 0.3
Combined seal	Conform	Faults	Downfaulted structures	0.6 - 0.8	0.5 – 0.6	0.3 - 0.5	0.1 - 0.3
	Conform	Facies shift	"shale out"	0.6 - 0.8	0.5 - 0.7	0.4 - 0.6	0.1 - 0.3
	Uncon -form	Conform	Subcrop structures	0.4 - 0.5	0.3 – 0.5	0.2 - 0.4	0.1 - 0.3

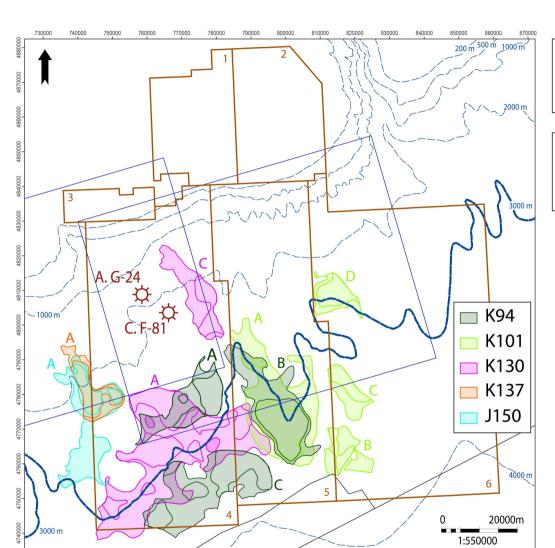
#### Trap: probability of presence of an efficient structural trap

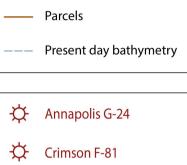
	Data reliability			2D Seismic	
Seismic correlation and mapping		3D Seismic	Dense grid size	Open grid size	Very open grid
	Low structural complexity	0.9 - 1.0	0.9 - 1.0	0.8 - 1.0	0.7 - 0.9
Good corr., nearby wells	High structural complexity	0.7 - 1.0	0.6 - 0.9	0.5 - 0.8	0.4 - 0.7
,	Low relief, uncertain depth conversion	0.6 - 0.9	0.5 - 0.8	0.4 - 0.7	0.3 - 0.6
	Low structural complexity	0.9 - 1.0	0.8 - 1.0	0.7 - 0.9	0.5 - 0.8
Uncertain corr, distant wells	High structural complexity	0.7 - 0.9	0.6 - 0.9	0.4 - 0.8	0.3 - 0.7
	Low relief, uncertain depth conversion	0.5 - 0.8	0.4 - 0.7	0.3 - 0.6	0.2 - 0.5
	Low structural complexity	0.9 - 1.0	0.7 - 1.0	0.6 - 0.8	0.4 - 0.7
Unreliable corr. Analogue Model	High structural complexity	0.4 - 0.7	0.3 - 0.6	0.2 - 0.5	0.1 - 0.4
	Low relief, uncertain depth conversion	0.3 - 0.7	0.2 - 0.6	0.1 - 0.5	0.1 - 0.4

-----

# **CHAPTER 8.2**

# **LEADS ASSESSMENT: Geophysical Methods**





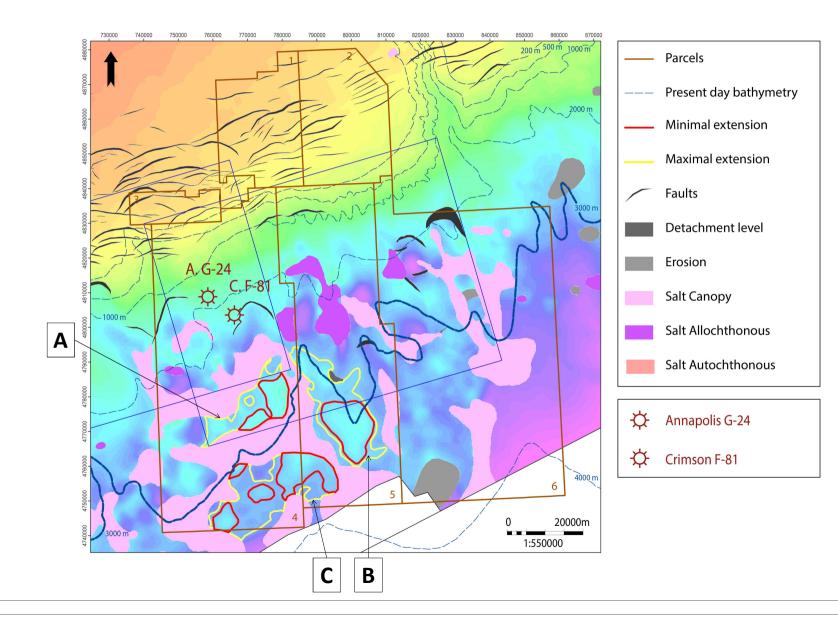
The map on the left shows the distribution of all leads picked for the lead assessment. Each lead is presented independently.

The slides are identically structured with :

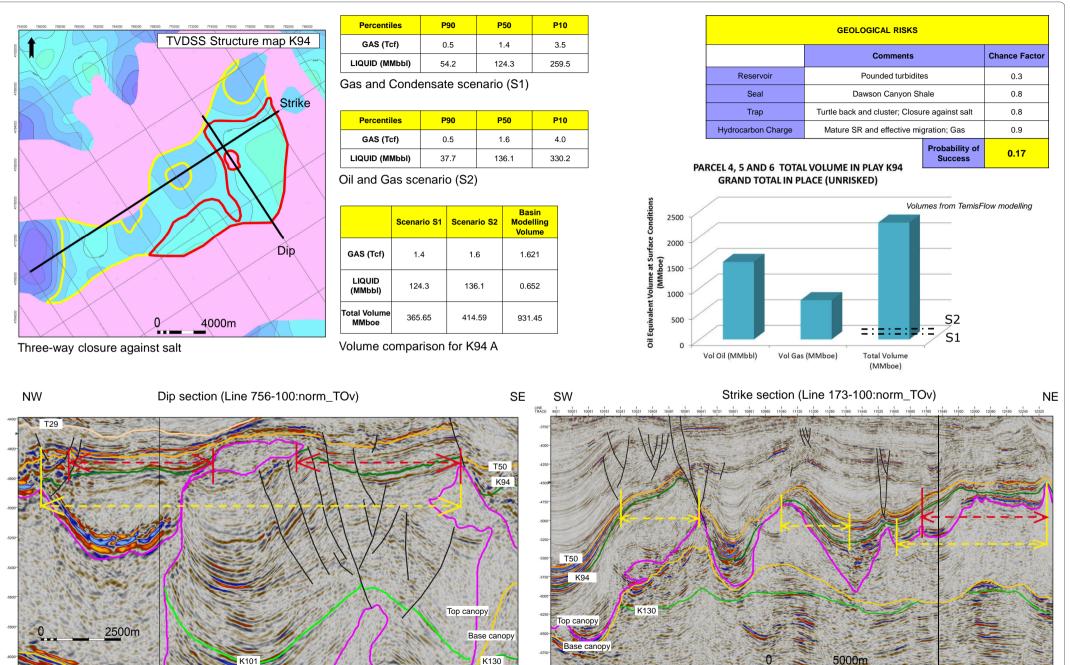
- a map showing the structure and its related closure on the upper right corner
- A table showing volumetric results for the Gas and Condensate scenario (S1)
- A table showing volumetric results for the Oil and Gas scenario (S2)
- A table comparing the P50 of each scenario to TemisFlow™ results for the same lead
- · A table on the upper right corner showing results from the risk assessment
- A figure showing the total hydrocarbon volume from TemisFlow™ modelling for the related play
- A dip and strike seismic line illustrating the structure, its closure and its maximum (yellow) and
  minimum (red) extent

Central Scotian Slope Study – CANADA – June 2016

# **ALL LEADS K94**



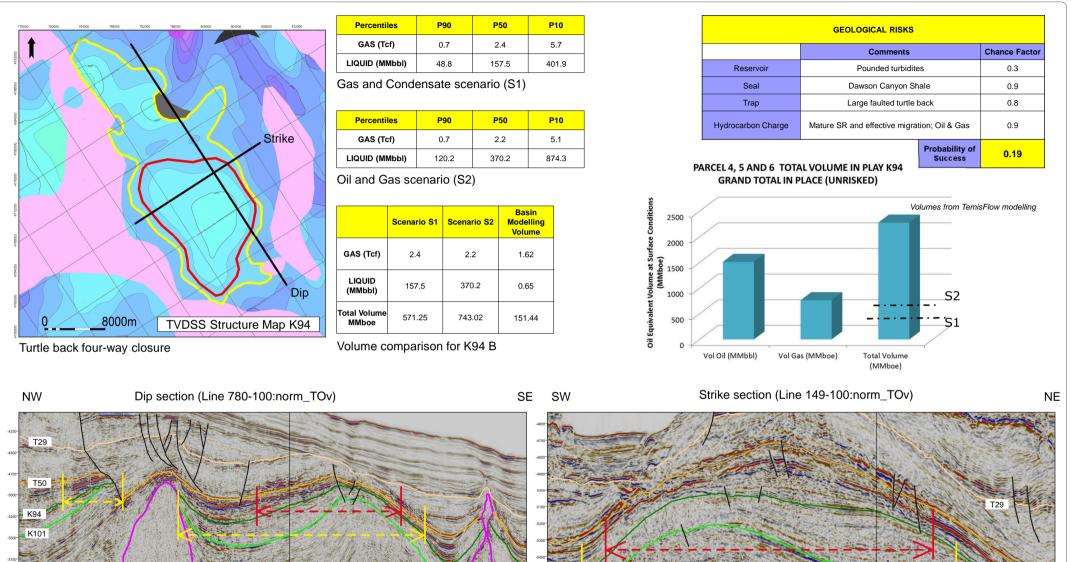
Central Scotian Slope Study – CANADA – June 2016



K94-A Lead Summary Plate

PL. 8.2.3

Central Scotian Slope Study – CANADA – June 2016



K130

Top canopy

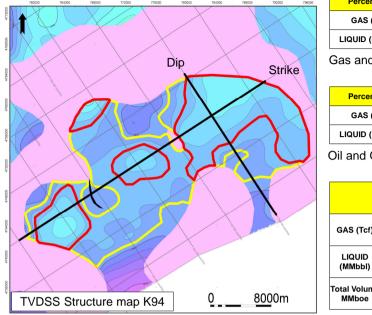
Base canopy

5000m

T50

K101

Central Scotian Slope Study - CANADA - June 2016



Three-way closures related to salt deformations (anticlines and turtle back)

Percentiles	P90	P50	P10
GAS (Tcf)	0.8	2.9	7.5
LIQUID (MMbbl)	58.4	195.1	496.2

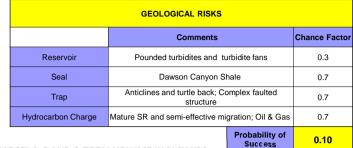
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	0.8	2.7	6.5
LIQUID (MMbbl)	162.6	469.1	1108.9

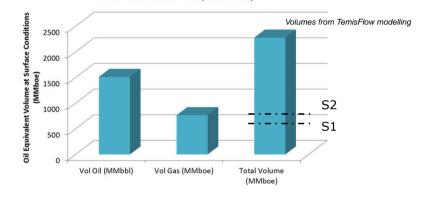
Oil and Gas scenario (S2)

	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	2.9	2.7	N/A
LIQUID (MMbbl)	195.1	469.1	N/A
Total Volume MMboe	696.87	930.97	N/A

Volume comparison for K94 C

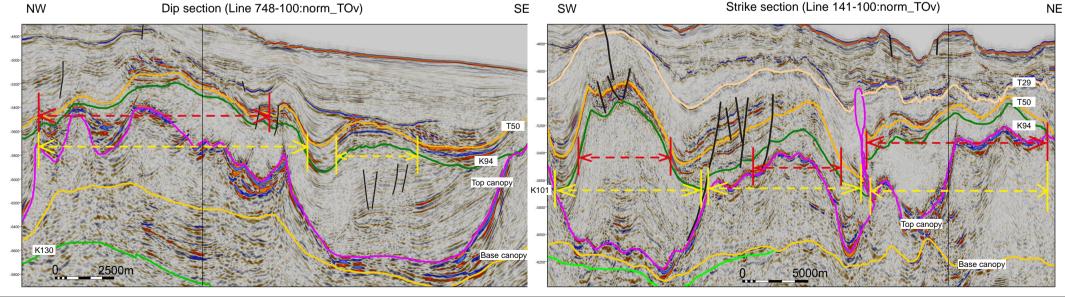


### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K94 **GRAND TOTAL IN PLACE (UNRISKED)**



Strike section (Line 141-100:norm\_TOv)

NE



SE

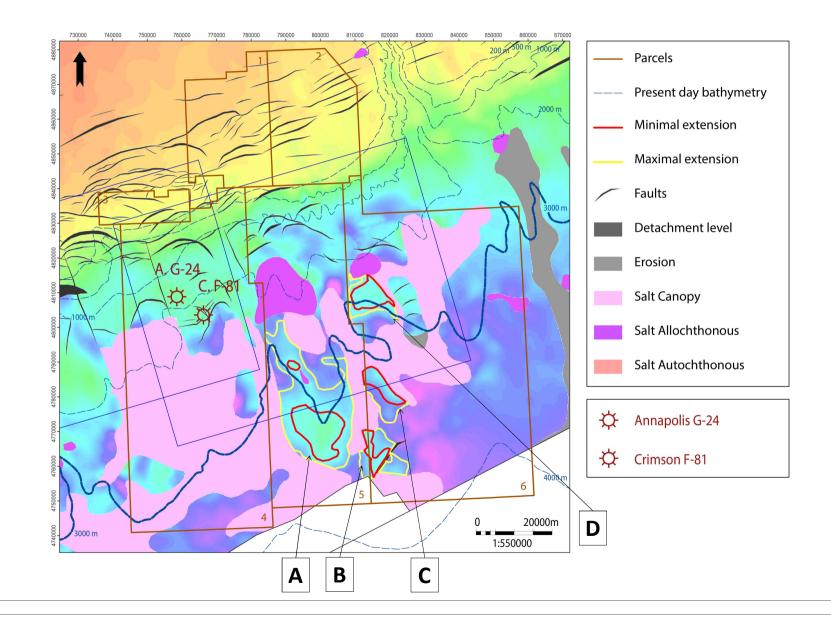
SW

# **K94-C Lead Summary Plate**

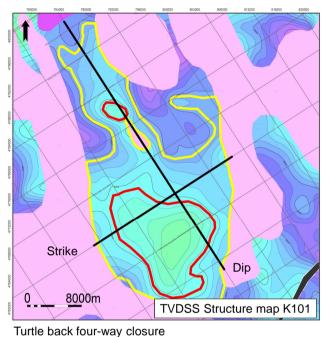
NW

Central Scotian Slope Study – CANADA – June 2016

# **ALL LEADS K101**



Central Scotian Slope Study – CANADA – June 2016



Percentiles	P90	P50	P90
GAS (Tcf)	1.5	5.0	12.3
LIQUID (MMbbl)	99.9	319.8	768.6

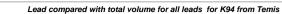
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	1.3	4.1	9.9
LIQUID (MMbbl)	271.6	771.9	1802.8

Oil and Gas scenario (S2)

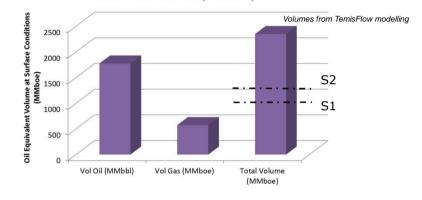
	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	5	4.1	1.535
LIQUID (MMbbl)	319.8	771.9	755.000
Total Volume MMboe	1181.77	1470.36	1019.63

Volume comparison for K101 A



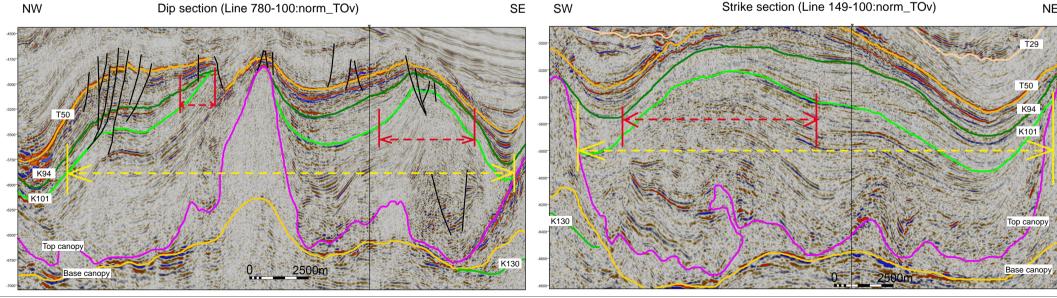
GEOLOGICAL RISKS					
	Comments	Chance Factor			
Reservoir	Pounded turbidites and turbidite fans		0.3		
Seal	Shortland Shale		0.9		
Тгар	Large faulted turtle back		0.8		
Hydrocarbon Charge	Mature SR and effective migration; Oil & Gas		0.9		
		Probability of Success	0.19		

### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K101 **GRAND TOTAL IN PLACE (UNRISKED)**



Strike section (Line 149-100:norm\_TOv)

NE

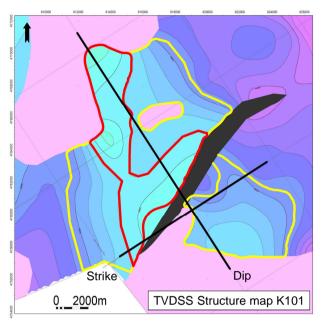


SE

SW

NW

Central Scotian Slope Study - CANADA - June 2016



Three-way closure against salt and fault

NW

Percentiles	P90	P50	P10
GAS (Tcf)	0.3	1.0	2.5
LIQUID (MMbbl)	22.9	68.6	168.2

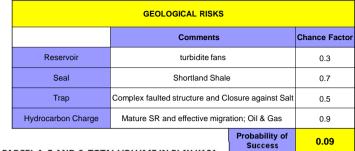
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	0.2	0.9	2.1
LIQUID (MMbbl)	53.8	163.3	386.0

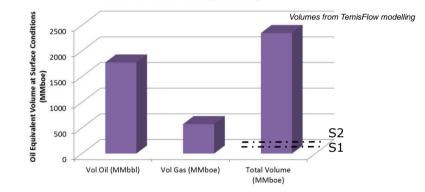
# Oil and Gas scenario (S2)

	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	1	0.9	N/A
LIQUID (MMbbl)	68.6	163.3	N/A
Total Volume MMboe	246.8	311.93	N/A

Volume comparison for K101 B

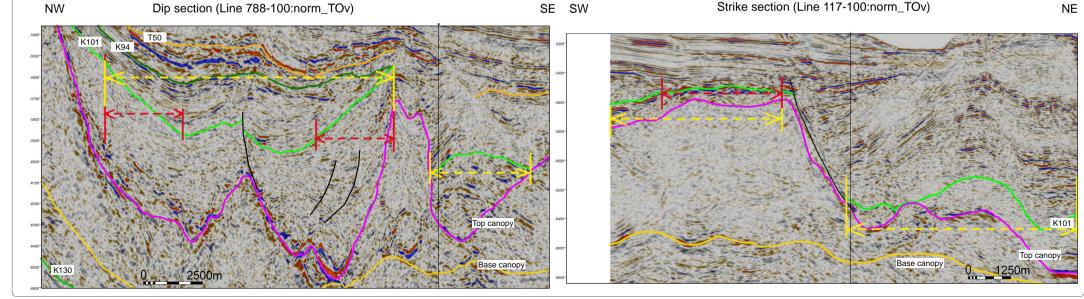


### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K101 **GRAND TOTAL IN PLACE (UNRISKED)**



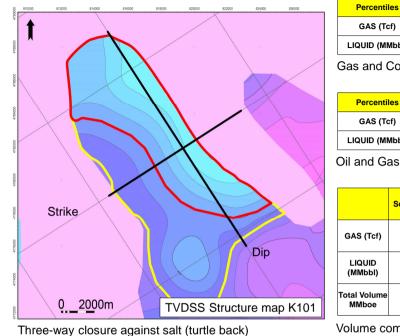
Strike section (Line 117-100:norm\_TOv)

NE



SE SW

Central Scotian Slope Study – CANADA – June 2016



Dip section (Line 804-100:norm\_TOv)

Percentiles	P90	P50	P10
GAS (Tcf)	0.3	0.9	2.2
LIQUID (MMbbl)	17.2	59.4	148.4

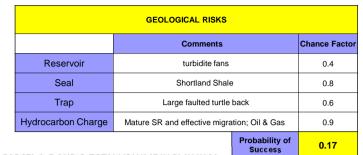
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	0.2	0.7	1.8
LIQUID (MMbbl)	48.1	138.6	320.5

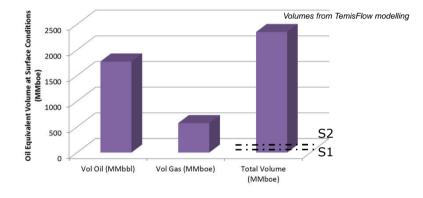
# Oil and Gas scenario (S2)

Scenario S1	Scenario S2	Basin Modelling Volume
0.9	0.7	N/A
59.4	138.6	N/A
212.17	264.84	N/A
	0.9	0.9         0.7           59.4         138.6

Volume comparison for K101 C

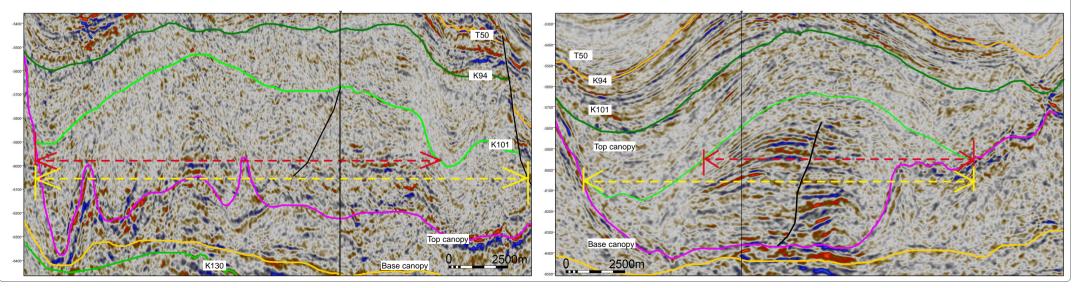


### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K101 GRAND TOTAL IN PLACE (UNRISKED)



Strike section (Line 141a-100:norm\_TOv)

NE

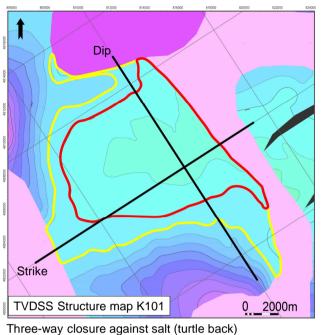


SE

SW

NW

Central Scotian Slope Study - CANADA - June 2016



Percentiles	P90	P50	P10
GAS (Tcf)	0.3	1.0	2.5
LIQUID (MMbbl)	22.1	66.7	157.8

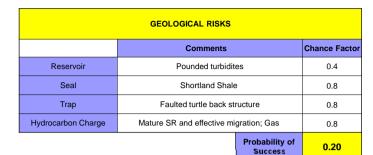
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	0.3	1.0	2.4
LIQUID (MMbbl)	31.0	84.7	199.7

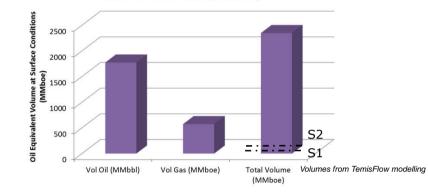
# Oil and Gas scenario (S2)

	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	1	1	0.114
LIQUID (MMbbl)	66.7	84.7	35.000
Total Volume MMboe	239.1	262.14	54.65

Volume comparison for K101 D

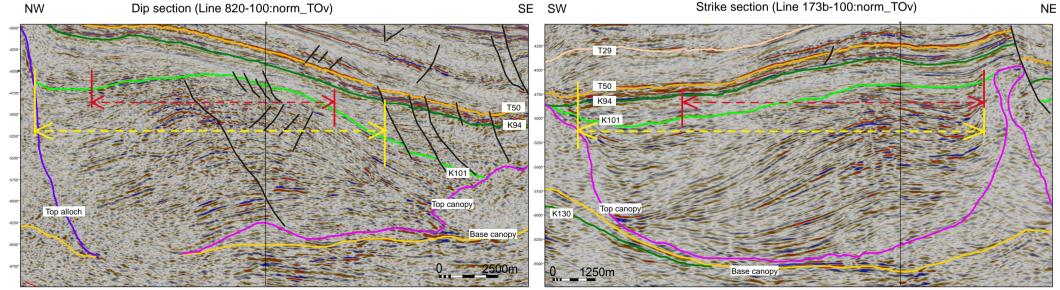


### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K101 **GRAND TOTAL IN PLACE (UNRISKED)**



# Strike section (Line 173b-100:norm\_TOv)

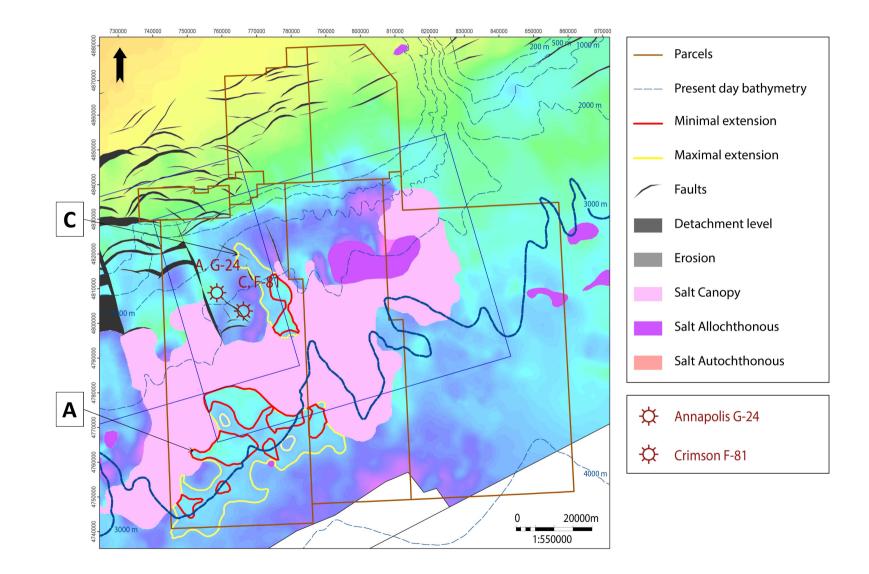
NE



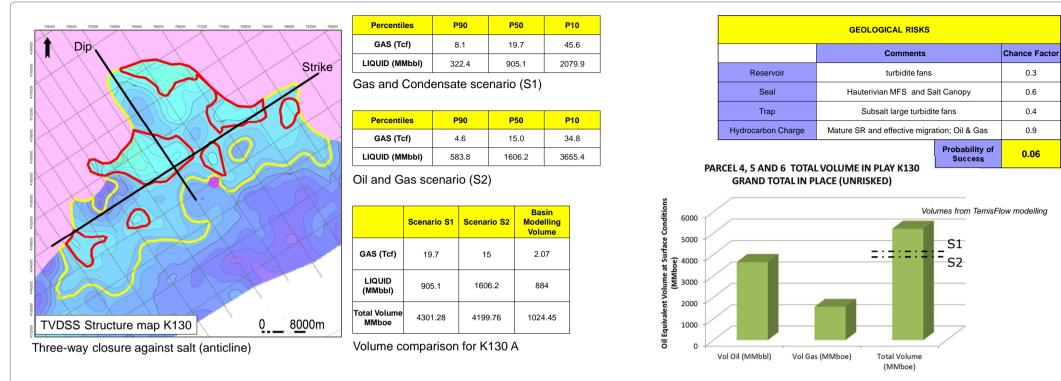
K101-D Lead Summary Plate

Central Scotian Slope Study – CANADA – June 2016

# **ALL LEADS K130**



Central Scotian Slope Study – CANADA – June 2016



NW

### Dip section (Line 732-100:norm\_TOv)

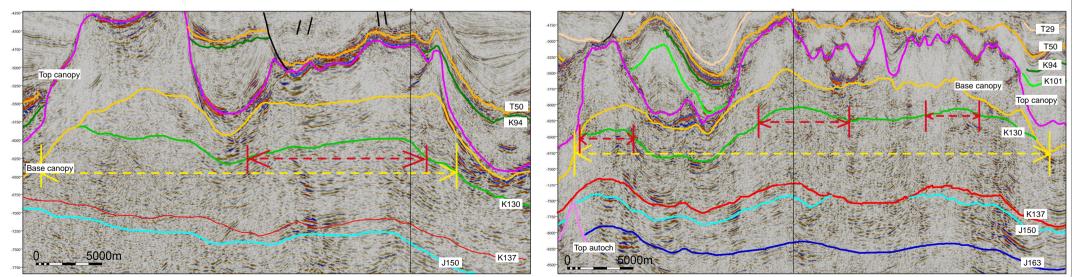


SW

SE

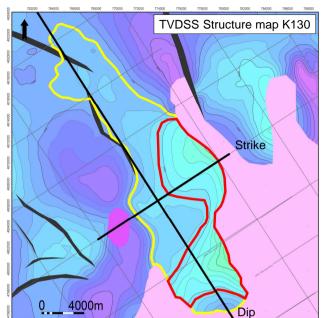


NE



K130-A Lead Summary Plate

Central Scotian Slope Study – CANADA – June 2016



Three-way closure against fault and salt (salt related	
anticline)	

Dip section (Line 772-100:norm\_TOv)

Percentiles	P90	P50	P10
GAS (Tcf)	1.9	4.7	9.8
LIQUID (MMbbl)	83.9	205.5	444.2

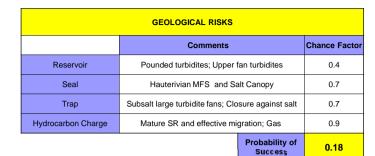
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10
GAS (Tcf)	1.9	4.7	10.4
LIQUID (MMbbl)	111.8	313.0	698.9

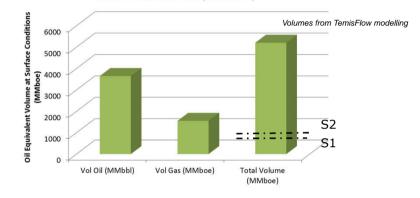
Oil and Gas scenario (S2)

	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	4.7	4.7	0.533
LIQUID (MMbbl)	205.5	313	95
Total Volume MMboe	1015.76	1117	186.89

Volume comparison for K130 C

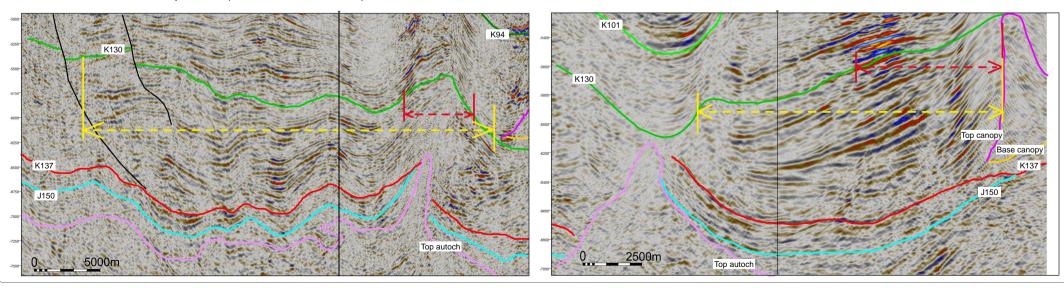


PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K130 GRAND TOTAL IN PLACE (UNRISKED)



# Strike section (Line 197-100:norm\_TOv)

NE



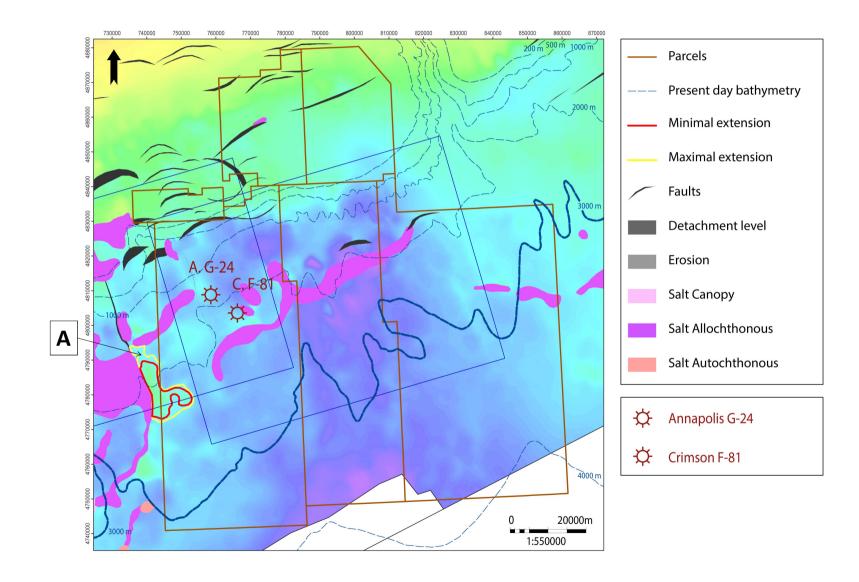
SE SW

K130-C Lead Summary plate

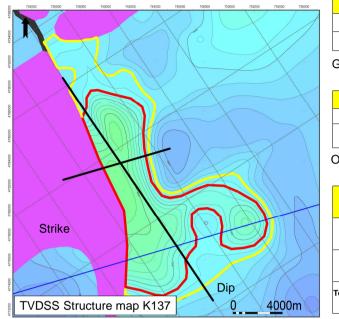
NW

Central Scotian Slope Study – CANADA – June 2016

# ALL LEADS K137



Central Scotian Slope Study - CANADA - June 2016



Three-way closure against salt (salt related anticline)

Percentiles	P90	P50	P10
GAS (Tcf)	0.1	0.2	0.3
LIQUID (MMbbl)	0.9	2.4	5.2

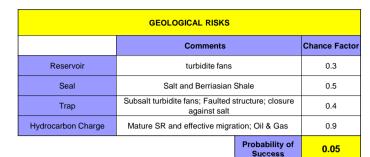
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10	
GAS (Tcf)	0.1	0.2	0.4	
LIQUID (MMbbl)	1.6	4.6	11.0	

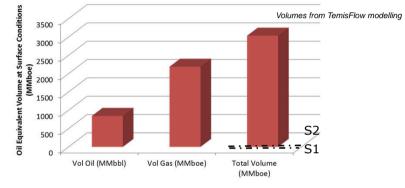
Oil and Gas scenario (S2)

	Scenario S1	Scenario S2	Basin Modelling Volume
GAS (Tcf)	0.2	0.2	0.187
LIQUID (MMbbl)	2.4	4.6	16
Total Volume MMboe	32.22	36.88	48.24

Volume comparison for K137 A

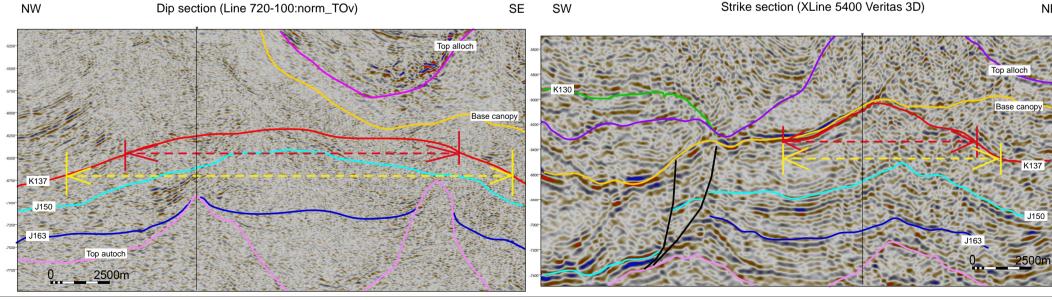


### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY K137 **GRAND TOTAL IN PLACE (UNRISKED)**



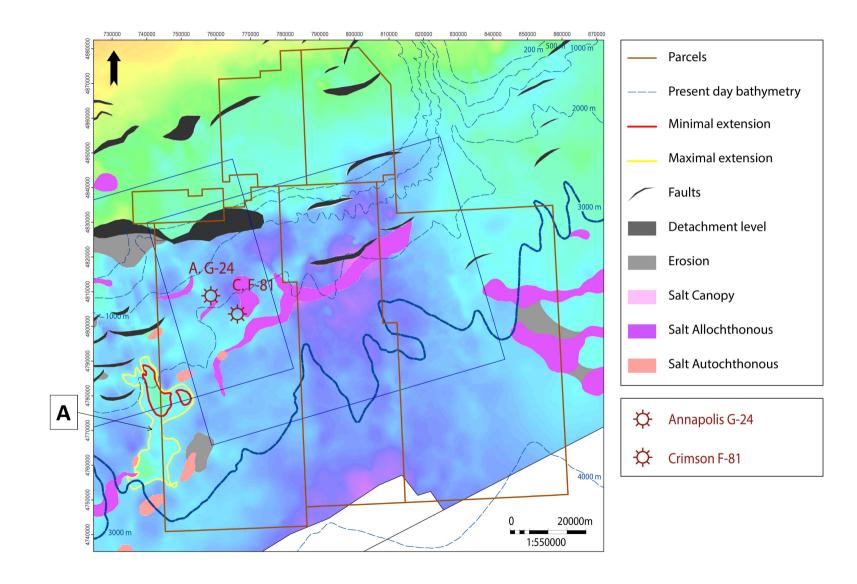
Strike section (XLine 5400 Veritas 3D)

NE

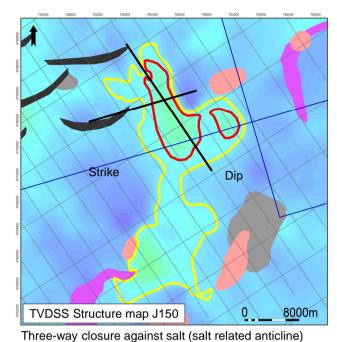


Central Scotian Slope Study – CANADA – June 2016

# **ALL LEADS J150**



Central Scotian Slope Study - CANADA - June 2016



	-		
Percentiles	P90	P50	P10
GAS (Tcf)	6.1	13.2	26.2
Condensates (MMbbl)	54.2	124.3	259.5
<u> </u>			

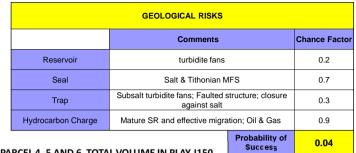
Gas and Condensate scenario (S1)

Percentiles	P90	P50	P10	
GAS (Tcf)	5.5	11.8	24.4	
LIQUID (MMbbl)	108.5	276.0	595.6	

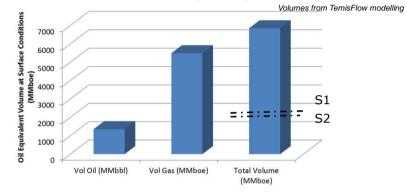
Oil and Gas scenario (S2)

	Scenario S1 Scenario S2		Basin Modelling Volume	
GAS (Tcf)	11.8 13.2		5.74	
LIQUID (MMbbl)	276	124.3	349	
Total Volume MMboe	2399.91	2307.51	1338.55	

Volume comparison for J150 A

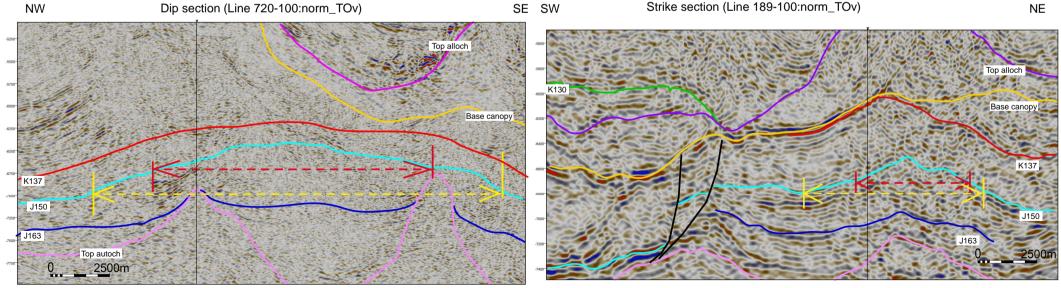


#### PARCEL 4, 5 AND 6 TOTAL VOLUME IN PLAY J150 **GRAND TOTAL IN PLACE (UNRISKED)**



# Strike section (Line 189-100:norm\_TOv)

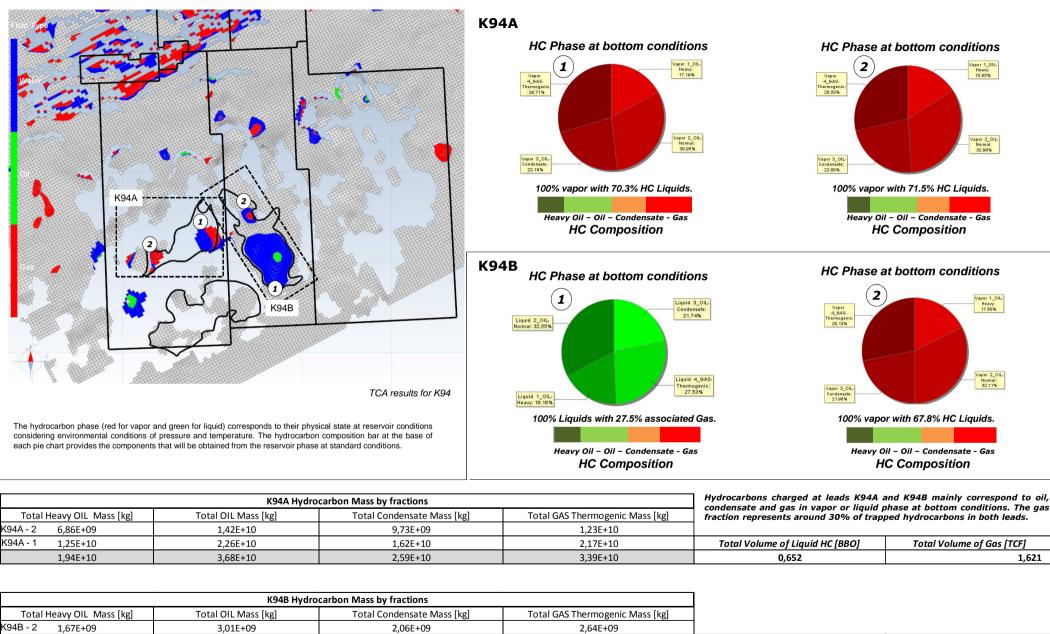
NE



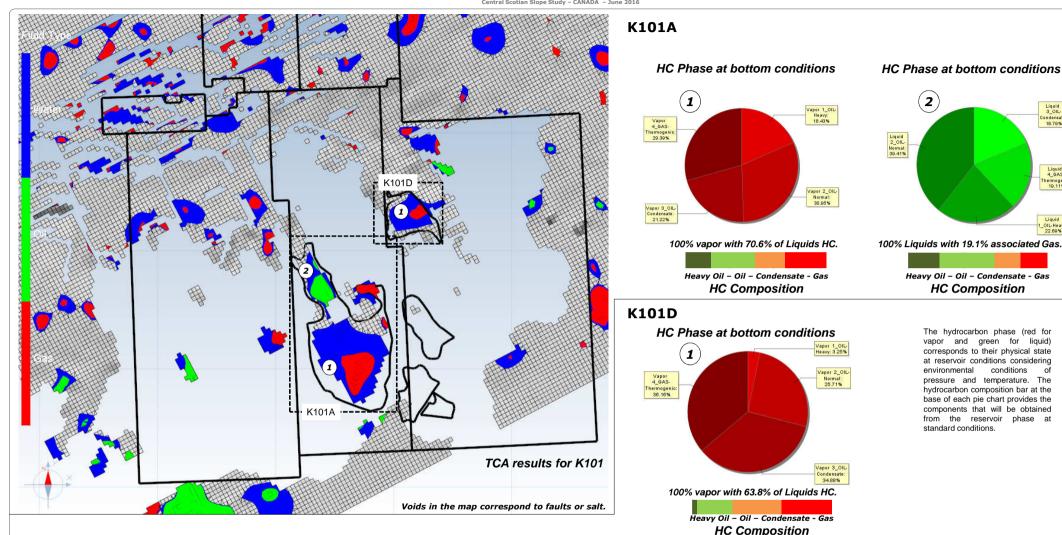
**CHAPTER 8.3** 

LEADS ASSESSMENT: Comparison with TemisFlow Results

Central Scotian Slope Study – CANADA – June 2016



K94B - 2	1,67E+09	3,01E+09	2,06E+09	2,64E+09		
K94B - 1	1,74E+09	3,11E+09	2,08E+09	2,63E+09	Total Volume of Liquid HC [BBO]	Total Volume of Gas [TCF]
	3,41E+09	6,13E+09	4,14E+09	5,27E+09	0,108	0,252



Hydrocarbons charged at leads K101A and K101D mainly correspond to oil, K101A Hydrocarbon Mass by fractions condensate and gas in vapor or liquid phase at bottom conditions. The gas Total Heavy OIL Mass [kg] Total OIL Mass [kg] Total Condensate Mass [kg] Total GAS Thermogenic Mass [kg] fraction present in lead K101A is around 19% to 30% of trapped volume. 1.79E+09 4.46E+09 3.08E+09 3.36E+09 The lead K101D, closer to the gas kitchen has around 35% of gas. 2,93E+08 5,96E+08 4,43E+08 5,60E+08 1,12E+10 1,95E+10 9,28E+09 9,44E+09 1,18E+10 1,98E+10 1,36E+10 1,88E+10 Total Volume of Liquid HC [BBO] Total Volume of Gas [TCF] 2,51E+10 4,43E+10 2,64E+10 3,21E+10 0,755 1,535 K101D Hydrocarbon Mass by fractions Total Heavy OIL Mass [kg] Total OIL Mass [kg] Total Condensate Mass [kg] Total GAS Thermogenic Mass [kg] Total Volume of Liquid HC [BBO] Total Volume of Gas [TCF] 2,14E+08 1,69E+09 2,30E+09 2,38E+09 0,035 0,114

Central Scotian Slope Study – CANADA – June 2016

Liquid 3\_OIL-Condensate 18.79%

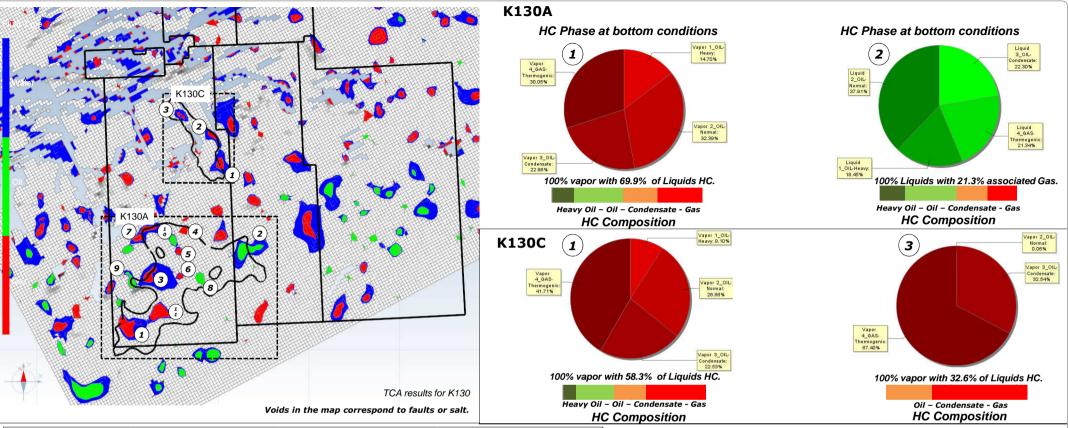
Liquid 4\_GAS-hermogenic 19.11%

Liquid 1\_0IL-Heavy: 22.69%

of

PL. 8.3.2





	K130A Hyd	rocarbon Mass by fractions	
Total Heavy OIL Mass [kg]	Total OIL Mass [kg]	Total Condensate Mass [kg]	Total GAS Thermogenic Mass [kg]
K130A - 6 2,30E+08	5,12E+08	5,45E+08	8,43E+08
K130A - 2 5,99E+09	1,23E+10	7,24E+09	6,93E+09
K130A - 4 5,93E+08	1,45E+09	1,02E+09	1,14E+09
K130A - 1 4,54E+09	1,00E+10	7,07E+09	9,29E+09
K130A - 5 7,26E+08	1,50E+09	1,02E+09	1,22E+09
K130A - 7 1,07E+09	3,06E+09	2,68E+09	3,94E+09
K130A - 10 1,07E+09	2,32E+09	1,50E+09	1,64E+09
K130A - 9 1,41E+09	3,24E+09	1,80E+09	1,94E+09
K130A - 3 1,77E+09	4,12E+09	3,55E+09	5,06E+09
K130A - 11 4,65E+09	9,41E+09	6,68E+09	8,76E+09
K130A - 8 2,03E+09	3,72E+09	2,22E+09	2,56E+09
2,41E+10	5,17E+10	3,53E+10	4,33E+10
	K130C Hyd	rocarbon Mass by fractions	
Total Heavy OIL Mass [kg]	Total OIL Mass [kg]	Total Condensate Mass [kg]	Total GAS Thermogenic Mass [kg]
K130C - 2 8,54E+07	1,64E+09	2,96E+09	5,34E+09
K130C - 1 9,49E+08	2,78E+09	2,35E+09	4,35E+09
<b>K130C - 3</b> 0	1,31E+06	7,07E+08	1,47E+09

6,01E+09

4,42E+09

1,03E+09

The hydrocarbon phase (red for vapor and green for liquid) corresponds to their physical state at reservoir conditions considering environmental conditions of pressure and temperature. The hydrocarbon composition bar at the base of each pie chart provides the components that will be obtained from the reservoir phase at standard conditions.

Hydrocarbons charged at leads K130A and K130C mainly correspond to oil, condensate and gas in vapor or liquid phase at bottom conditions. The gas fraction present in lead K130A is around 21% to 30% of the trapped volume. The lead K130C, closer to the gas kitchen has a gas content of around 40% to 67%.

Total Volume of Gas [TCF]

Total Volume of Gas [TCF]

2,069

0,533

Total Volume of Liquid HC [BBO]

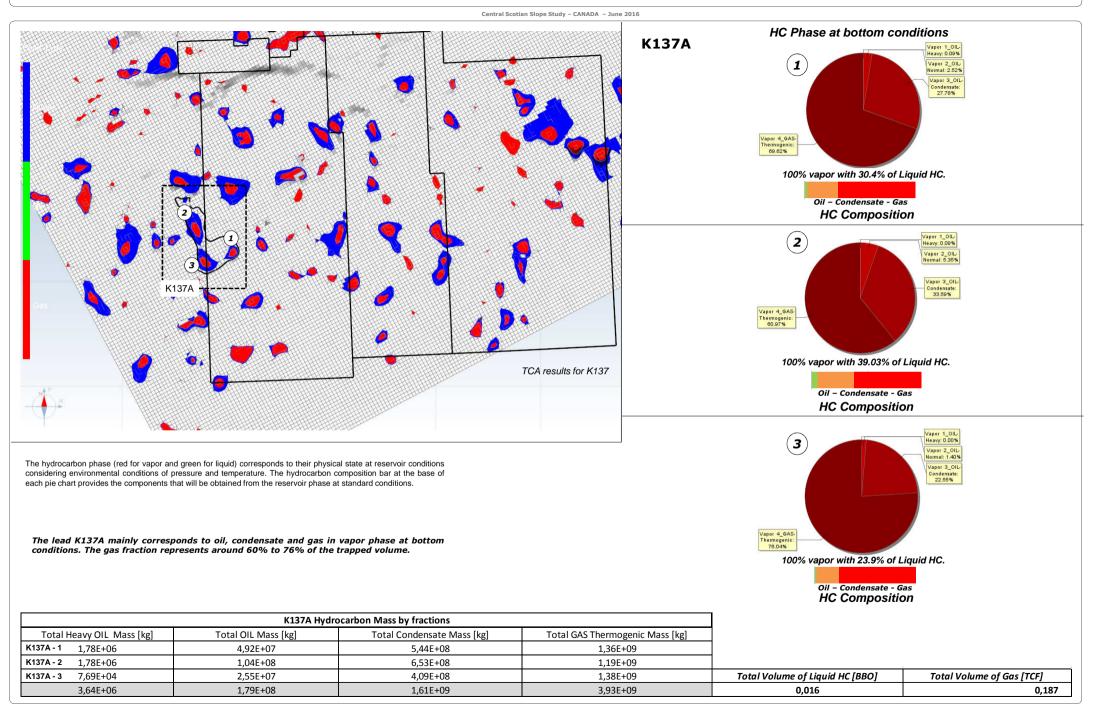
0,884

Total Volume of Liquid HC [BBO]

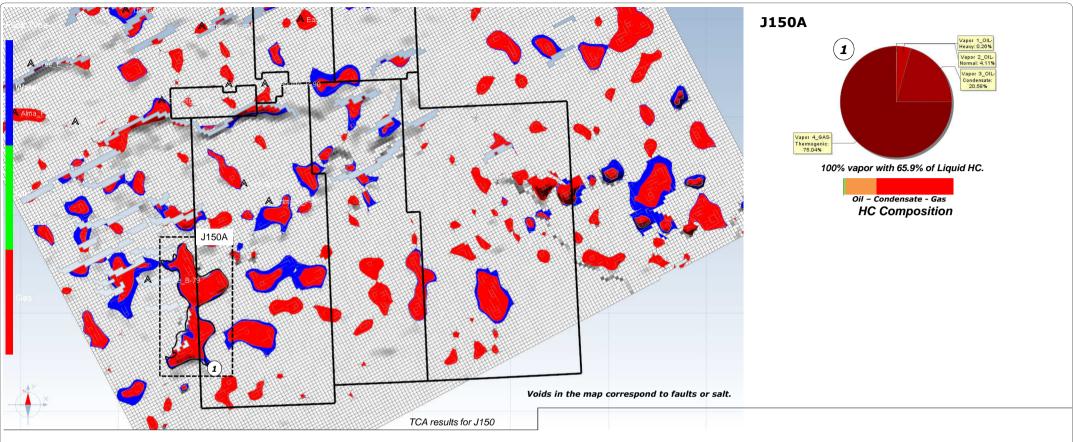
0,095

Lead Assessment – K	(130A	and	K130C
---------------------	-------	-----	-------

1,12E+10



Central Scotian Slope Study – CANADA – June 2016



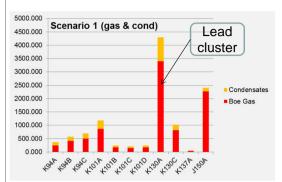
The hydrocarbon phase (red for vapor and green for liquid) corresponds to their physical state at reservoir conditions considering environmental conditions of pressure and temperature. The hydrocarbon composition bar at the base of each pie chart provides the components that will be obtained from the reservoir phase at standard conditions.

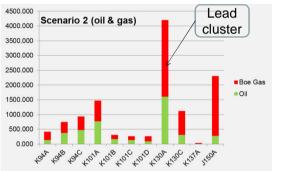
The lead K150A mainly corresponds to oil, condensate and gas in vapor phase at bottom conditions. The gas fraction represents 75% of the trapped volume.

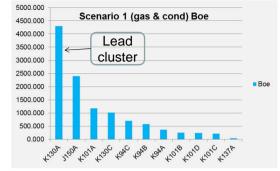
	J150A Hydro				
Total Heavy OIL Mass [kg]	Total OIL Mass [kg]	Total Condensate Mass [kg]	Total GAS Thermogenic Mass [kg]	Total Volume of Liquid HC [BBO]	Total Volume of Gas [TCF]
K150A - 1 4,23E+08	6,58E+09	3,30E+10	1,20E+11	0,349	5,740

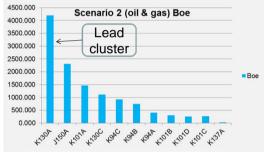
Central Scotian Slope Study – CANADA – June 2016

#### Graphics showing volumes per lead (left) and lead ranking (right) for both scenarios (Gas and Condensate vs Oil and Gas)









#### Table 1: Resources summary by stratigraphic position. Grand totals are shown in MMbbl in the last row

		Gas & Condensates (S1)			Oil & Gas (S2)			TemisFlow					
Play	Lead#	Gas	Boe Gas	Condensates	Boe	Gas	Boe Gas	Oil	Boe	Gas	Boe Gas	Liquid	Boe
		Tcf	MMbbl	MMbbl	MMbbl	Tcf	MMbbl	MMbbl	MMbbl	Tcf	MMbbl	MMbbl	MMbbl
	K94A	1.40	241.35	124.30	365.65	1.62	278.46	136.13	414.59	1.62	279.45	652	931.45
K94	K94B	2.40	413.75	157.50	571.25	2.16	372.77	370.24	743.02	0.25	43.44	108	151.44
	K94C	2.91	501.74	195.13	696.87	2.68	461.83	469.14	930.97	-	-	-	-
	K101A	5.00	861.97	319.80	1181.77	4.05	698.48	771.88	1470.36	1.54	264.63	755	1019.63
K101	K101B	1.03	178.21	68.59	246.80	0.86	148.59	163.33	311.93	-	-	-	-
KIUI	K101C	0.89	152.72	59.45	212.17	0.73	126.21	138.64	264.84	-	-	-	-
	K101D	1.00	172.39	66.70	239.09	1.03	177.45	84.69	262.14	0.11	19.65	35	54.65
130	K130A	19.70	3396.18	905.10	4301.28	15.04	2593.56	1606.20	4199.76	2,07	356,86	884	1240,85 7
100	K130C	4.70	810.26	205.50	1015.76	4.66	803.97	313.03	1117.00	0.53	91.89	95	186.89
137	K137A	0.20	34.48	2.40	36.88	0.16	27.67	4.55	32.22	0.19	32.24	16	48.24
150	J150A	13.20	2275.61	124.30	2399.91	11.78	2031.47	276.04	2307.51	5.74	989.55	349	1338.55
	Total	52.43	9038.66	2228.77	11267.43	44.78	7720.46	4333.89	12054.35	12,05	2077.70	2894	4971.7

#### Leads Ranking

A summary of leads assessment from both the conventional geophysical and TemisFlow modelling approaches is presented here.

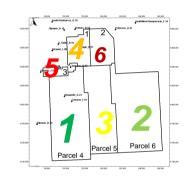
Results from the conventional geophysical approach are shown on the graphics on the left and volumes are summarized in Table 1. Results show a large range of values for both Oil and Gas, with similar results for Scenario 1 and 2. Gas values range from 0.2 Tcf (K137) to 15-19 Tcf (K130A) with most of the values around 2 to 4 Tcf. Oil values range from 2-4 MMbbl (K137) to 1600 MMbbl (K130A) with most of the values between 140 to 470 MMbbl. It should be noted that some large volumes are linked to lead clusters such as the K130A.

Results of the lead assessment from TemisFlow basin modelling is presented below and compared to the geophysical approach in Table 1. Total volumes for oil and for gas are presented for each parcel and for each play (Table 2). Results show a large range of values for both Oil and Gas, with the largest volumes in deep water. Gas values range from 5 Tcf (parcel 3) to 28 Tcf (Parcel 4). Oil values range from 392 MMbbl (Parcel 2) to 3762 MMbbl (Parcel 4) with again the largest volumes in deep water.

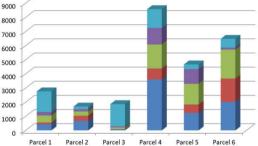
Parcels ranking shows that deep water parcels rank better than those on the shelf, with Parcel 4 as the most attractive area. When expressed into volume per surface unit, Parcel 1 in the shelf appears to be the most attractive, but Parcel 4 still ranks second (see also Chapter 7, PL. 7.3.25).

#### Key numbers: Total ~ 12 bnbbls liquids + 80 tcf gas (~26 mmboe)

ē







Parcel ranking per volume

Table 2: TemisFlow Grand Total Volume and volume per Surface Area for all leads within each parcel Grand Total

#### Volume per Surface Area

Parcels	Vol Gas (Tcf)	Vol Oil (MMbbl)	Total Volume (MMboe)	Vol Gas (bcf/km²)	Vol Oil (Mbbl/km²)	Total Volume (Mboe/km²)
Parcel 1	7	1512	2760	31	6418	11718
Parcel 2	8	392	1689	10	501	2158
Parcel 3	5	1072	1859	5	1144	1984
Parcel 4	28	3762	8576	8	1031	2350
Parcel 5	15	2063	4667	6	799	1807
Parcel 6	18	3319	6477	1	270	528
Total Parcels	81	12120	26028	4	592	1272

PL. 8.3.6

#### **HC Resource Summary**